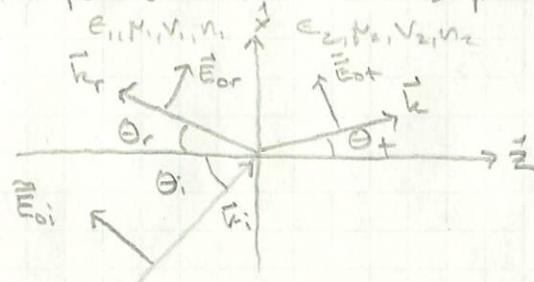


# Fresnel Equations

(I)

For polarizations in the  $x-z$  plane:



$$\text{we have: } \tilde{E}_{oi} = \tilde{E}_{oi} e^{i(\vec{k}_i \cdot \vec{r} - \omega t)}$$

$$\tilde{E}_{or} = \tilde{E}_{or} e^{i(\vec{k}_r \cdot \vec{r} - \omega t)}$$

$$\tilde{E}_{ot} = \tilde{E}_{ot} e^{i(\vec{k}_t \cdot \vec{r} - \omega t)}$$

$$\perp \text{ imposed: } E_1 E_1^+ = E_2 E_2^+ \text{ at } z=0 \quad (*)$$

$$\tilde{E}_1'' = \tilde{E}_2'' \text{ at } z=0 \quad (o)$$

to get 1.  $\vec{k}_i, \vec{k}_r, \vec{k}_t$  lie in a plane  
2.  $\theta_r = \theta_i$

$$3. \sin \theta_t = \frac{n_1}{n_2} \sin \theta_i$$

$$\text{by using } \tilde{E}_{oi} = \tilde{E}_{oi} (\cos \theta_i \hat{x} - \sin \theta_i \hat{z})$$

$$\tilde{E}_{or} = \tilde{E}_{or} (\cos \theta_i \hat{x} + \sin \theta_i \hat{z})$$

$$\tilde{E}_{ot} = \tilde{E}_{ot} (\cos \theta_t \hat{x} - \sin \theta_t \hat{z})$$

$$\therefore (*) : E_1 (-\tilde{E}_{oi} \sin \theta_i + \tilde{E}_{or} \sin \theta_r) = E_2 \tilde{E}_{ot} \sin \theta_t$$

$$\tilde{E}_{oi} \cos \theta_i + \tilde{E}_{or} \cos \theta_r = \tilde{E}_{ot} \cos \theta_t$$

now from 2. & 3., these read:

$$(\tilde{E}_{oi} - \tilde{E}_{or}) = \frac{E_2}{E_1} \cdot \frac{n_1}{n_2} \tilde{E}_{ot}$$

$$= \frac{\mu_1 \nu_1}{\mu_2 \nu_2} = \beta.$$

$$(\tilde{E}_{oi} + \tilde{E}_{or}) = \frac{\cos \theta_t}{\cos \theta_i} \tilde{E}_{ot}$$

$$= \alpha$$

$$\text{add 'em: } 2\tilde{E}_{oi} = (\alpha + \beta) \tilde{E}_{ot} \Rightarrow \tilde{E}_{ot} = \frac{2}{\alpha + \beta} \tilde{E}_{oi}$$

$$\text{subtract: } 2\tilde{E}_{or} = (\alpha - \beta) \tilde{E}_{ot} = \frac{2(\alpha - \beta)}{\alpha + \beta} \tilde{E}_{ot}$$

$$\text{Fresnel eqns: } \tilde{E}_{or} = \frac{\alpha - \beta}{\alpha + \beta} \tilde{E}_{oi}; \quad \tilde{E}_{ot} = \frac{2}{\alpha + \beta} \tilde{E}_{oi}$$

note: •  $\tilde{E}_{ot}$  is in the same direction as  $\tilde{E}_{oi}$ , b+t  $\tilde{E}_{or}$  could be opposite  $\tilde{E}_{oi}$  - upside down.

•  $\beta$  is a constant, but  $\alpha = \frac{\cos \theta_t}{\cos \theta_i}$  depends on  $\theta_i$ .

$$\alpha = \frac{1 - \sin^2 \theta_t}{\cos \theta_i} = \frac{1 - (\frac{n_1}{n_2} \sin \theta_i)^2}{\cos \theta_i}$$

• as  $\theta_i \rightarrow \pi/2$ ,  $\alpha \rightarrow \infty$  &  $\tilde{E}_{or} \rightarrow \tilde{E}_{oi}$   
all the incident wave is reflected



- $\tilde{E}_{or} = 0$  if  $\alpha = \beta$ , the incident angle is called "Brewster's angle"

$$1 - \left(\frac{n_1}{n_2}\right)^2 \sin^2 \Theta_i = \beta^2 \cos^2 \Theta_i = \beta^2 (1 - \sin^2 \Theta_i)$$

so

$$\sin^2 \Theta_i = \frac{\beta^2 - 1}{\beta^2 + \left(\frac{n_1}{n_2}\right)^2}$$

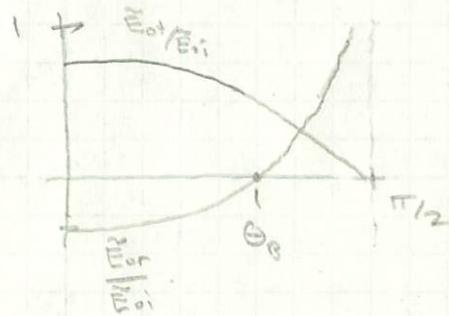
- at  $\Theta_i = 0$ ,  $\alpha = 1 \Rightarrow \tilde{E}_{or} = \frac{1-\beta}{1+\beta} \tilde{E}_{oi}$

$$\tilde{E}_{or} = \frac{2}{1+\beta} \tilde{E}_{oi}$$

for  $\beta = \frac{\mu_1 n_1}{\mu_2 n_2} = \frac{n_2}{n_1}$ , if  $n_2 > n_1$ ,  $\tilde{E}_{or} < 0$

"often"

take  $n_1 = 1$ ,  $n_2 > 1$  (air to water), the coefficient ratios can be sketched as function of  $\Theta_i$ :



Intensities:  $\vec{I} = \frac{1}{2} \epsilon_0 V^2 \hat{k}$  in general.

the intensity entering the interface from the incident wave is:

$$\vec{I} \cdot \hat{z} = \frac{1}{2} \epsilon_0 V_i \tilde{E}_{oi}^2 \cos \Theta_i \quad \text{or} \quad \hat{z} \cdot \hat{h}_i = \omega \Theta_i$$

The reflected intensity is:

$$\vec{I}_r \cdot \hat{z} = \frac{1}{2} \epsilon_0 V_i \tilde{E}_{or}^2 \cos \Theta_r = I_r$$

& the transmitted piece is

$$\vec{I}_t \cdot \hat{z} = \frac{1}{2} \epsilon_0 V_2 \tilde{E}_{ot}^2 \cos \Theta_t = I_t$$

we can take the ratios:

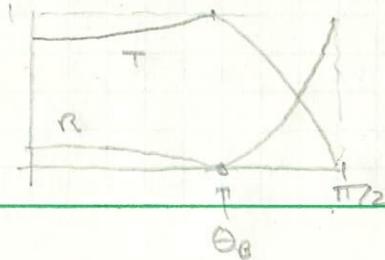
$$R = \frac{I_r}{I_i} = \frac{\tilde{E}_{or}^2}{\tilde{E}_{oi}^2} = \left( \frac{\alpha - \beta}{\alpha + \beta} \right)^2$$

$$T = \frac{I_t}{I_i} = \frac{\epsilon_2 V_2 \tilde{E}_{ot}^2 \cos \Theta_t}{\epsilon_1 V_i \tilde{E}_{oi}^2 \cos \Theta_i} = \alpha \beta \cdot \left( \frac{2}{\alpha + \beta} \right)^2$$

conservation of energy requires:

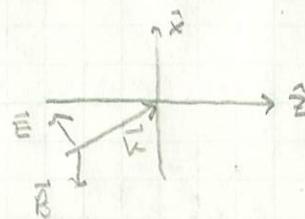
$$R + T = 1 \quad \text{check: } \frac{\alpha^2 - 2\alpha\beta + \beta^2 + 4\alpha\beta}{(\alpha + \beta)^2} = \frac{(\alpha + \beta)^2}{(\alpha + \beta)^2} = 1 \quad \checkmark$$

a sketch of R, T as functions of  $\Theta_i$  looks like:



## Wave Guides

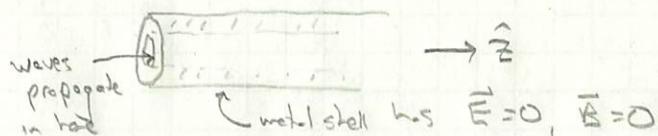
Our plane waves are infinite sheets:



We know that this is an approximation valid for radiation far from a dipole source:



We can localize plane waves using conducting boundaries:



The b.c. is, then,  $\vec{E}''=0$  at the surface

$$\vec{B}''=0$$

(to keep the conductor at equipotential, since current will move around, so we don't have  $E^1=0$  or  $B^1=0$  necessarily.)

Assume we have a monochromatic plane wave travelling in the  $\hat{z}$  direction.

$$\tilde{\vec{E}} = \tilde{\vec{E}}_0(x, y) e^{i(hz - \omega t)} \quad \tilde{\vec{B}} = \tilde{\vec{B}}_0(x, y) e^{i(hz - \omega t)}$$

$$\omega = hc$$

$$\nabla \cdot \tilde{\vec{E}}_0 = E_x \hat{x} + E_y \hat{y} + E_z \hat{z}, \quad \tilde{\vec{B}}_0 = B_x \hat{x} + B_y \hat{y} + B_z \hat{z}.$$

↑ complex  
in general

The vacuum Maxwell's eqns are

$$\nabla \cdot \tilde{\vec{E}} = 0 \quad \nabla \times \tilde{\vec{E}} = -\frac{\partial \tilde{\vec{B}}}{\partial t} \quad \nabla \cdot \tilde{\vec{B}} = 0 \quad \nabla \times \tilde{\vec{B}} = \frac{1}{c^2} \frac{\partial \tilde{\vec{E}}}{\partial t} \quad (*)$$

so we know the wave eqn. will emerge in the usual way — or assumed form already satisfied the wave eqn. ✓

How does the full set in (\*) constrain the functions in  $\tilde{\vec{E}}_0$  &  $\tilde{\vec{B}}_0$ ?

$$\nabla \times \tilde{\vec{E}} = -\frac{\partial \tilde{\vec{B}}}{\partial t} \Rightarrow (\frac{\partial E_y}{\partial z} - \frac{\partial E_z}{\partial y}) \hat{x} + (\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x}) \hat{y} + (\frac{\partial E_x}{\partial y} - \frac{\partial E_y}{\partial x}) \hat{z}$$

$$= +i\omega [B_x \hat{x} + B_y \hat{y} + B_z \hat{z}]$$

so get 3 eqns that can be used to relate  $E_x, B_x, E_y, B_y$  to  $E_z, B_z$  & their derivatives.

Then those 2 are governed by:

$$[\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + (\omega/c)^2 - k^2] E_z = 0 \quad \leftarrow \text{longitudinal component}$$

$$[\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + (\omega/c)^2 - k^2] B_z = 0 \quad \leftarrow$$

If  $E_z = 0$ , there are "transverse electric" waves, if  $B_z = 0$ , they are "transverse magnetic" waves — if  $E_z = 0 \wedge B_z = 0$ , they are "TEM" waves → these cannot occur for our setup. Since:  $\nabla \cdot \tilde{\vec{E}} = 0 \rightarrow \nabla \times \tilde{\vec{E}} = 0 \Rightarrow \nabla^2 V = 0$

so  $V$  has max/min only at the boundary — that boundary is on equipotential, so  $V$  has constant value throughout the cavity, & therefore  $\tilde{\vec{E}} = 0$ . ✓