

Linear Materials

(H)

For linear materials w/ $\vec{D} = \epsilon \vec{E}$, $\vec{H} = \frac{1}{\mu} \vec{B}$,
Maxwell's eqns read:

$$\nabla \cdot \vec{D} = \rho_f$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{H} = \frac{1}{\mu_f} \vec{J}_f + \frac{\partial \vec{D}}{\partial t}$$

& in free-charge "vacuum":

$$\nabla \cdot \vec{E} = 0 \quad \nabla \times \vec{E}^1 = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \cdot \vec{B} = 0 \quad \nabla \times \vec{B} = \mu_0 \frac{\partial \vec{E}}{\partial t} = \epsilon_0 \nu^2$$

we set $n = \epsilon_r > 1$, the "index of refraction"

$$n = \sqrt{\frac{\mu_r \epsilon_r}{\mu_0 \epsilon_0}} \approx \sqrt{\frac{\epsilon_r}{\epsilon_0}} = \epsilon_r \text{ "dielectric const."}$$

$\epsilon_r \approx 1$ for many materials.

plane wave solutions to the set in (*) have

$$u = k \epsilon \vec{E}^2 + \frac{1}{2\mu} \vec{B}^2$$

$$\vec{s} = \frac{1}{\mu} \vec{E} \times \vec{B}$$

w/ "the usual" $B \sim \frac{1}{\nu} E$, so the intensity

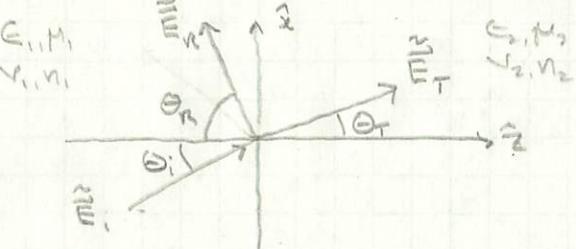
$$I = \langle \vec{s} \rangle = \frac{1}{2} \frac{1}{\mu} \nu^2 E^2 = k \epsilon \nu E^2$$

We will be interested in what happens to a wave that moves from one medium into another, & the boundary conditions will be important!

$$\begin{array}{l} E_1, \mu_1 \\ \downarrow \\ \vec{E} \\ \uparrow \\ E_2, \mu_2 \end{array} \quad \begin{array}{l} \epsilon_1, \epsilon_1^\perp = \epsilon_2 \epsilon_2^\perp \\ \vec{E}_1^\parallel = \vec{E}_2^\parallel \\ B_1^\perp = B_2^\perp \\ \frac{1}{\mu_1} \vec{B}_1^\parallel = \frac{1}{\mu_2} \vec{B}_2^\parallel \end{array}$$

Reflection & Transmission

The story: A plane wave comes in from the left, runs into a medium change, that gives rise to a reflected wave & a transmitted wave.



$$\vec{E}_i = \vec{E}_{0i} e^{i(\vec{k}_i \cdot \vec{r} - \omega t)} \quad \text{w/ } k_i v_i = \omega$$

$$\vec{B}_i = \frac{1}{\nu_i} \hat{n}_i \times \vec{E}_i$$

$$\vec{E}_r = \vec{E}_{0r} e^{i(\vec{k}_r \cdot \vec{r} - \omega t)}$$

$$\vec{B}_r = \frac{1}{\nu_r} \hat{n}_r \times \vec{E}_r$$

$$\vec{E}_+ = \vec{E}_{0+} e^{i(\vec{k}_+ \cdot \vec{r} - \omega t)}$$

$$\vec{B}_+ = \frac{1}{\nu_2} \hat{n}_+ \times \vec{E}_+$$

$$(k_r v_r = \omega)$$

$(k_r v_r = \omega)$? Why is ω fixed?

On the left, the total electric field is the sum of the incident + reflected fields.

The general structure of the boundary conditions

$$\underline{e}^{i(\vec{k}_i \cdot \vec{r} - \omega t)} + \underline{e}^{i(\vec{k}_r \cdot \vec{r} - \omega t)} = \underline{e}^{i(\vec{k}_t \cdot \vec{r} - \omega t)} \quad (*)$$

wl $\vec{n} = \hat{x} + \hat{y}$. The $e^{-i\omega t}$ piece will cancel,

$$\vec{k}_i \cdot \vec{r} = k_{ix} \hat{x} + k_{iy} \hat{y}$$

$$\vec{k}_r \cdot \vec{r} = k_{rx} \hat{x} + k_{ry} \hat{y}$$

In order for (*) to hold $\nabla \times \vec{E} \rightarrow \hat{y}$, we must have

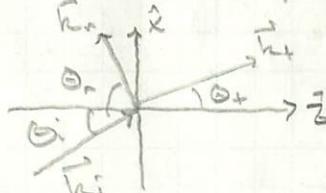
$$k_{ix} = k_{rx} = k_{tx} \rightarrow k_{iy} = k_{ry} = k_{ty}$$

Suppose \vec{k}_i lies in the xz plane, wl $k_{iy} = 0$, then

$$k_{iy} = 0 \rightarrow k_{ty} = 0$$

so that $\vec{k}_r + \vec{k}_t$ also lie in the xz plane

1. incident, reflected + transmitted wave vectors lie in $\hat{0}$ plane.



$$\begin{aligned} \vec{k}_i &= k_{ix} \hat{x} + k_{iz} \hat{z} \\ &= k_i \sin \theta_i \hat{x} + k_i \cos \theta_i \hat{z} \end{aligned}$$

$$wl \quad k_i v_i = \omega$$

$$\text{and } \vec{k}_{ir} = k_{rx} \hat{x} + k_{rz} \hat{z}$$

$$= k_r \sin \theta_r \hat{x} - k_r \cos \theta_r \hat{z}$$

$$wl \quad k_r v_i = \omega \Rightarrow k_i = k_r, \text{ so}$$

2. $\sin \theta_i = \sin \theta_r$, angle of incidence equals angle of reflection
 $\theta_i = \theta_r$.

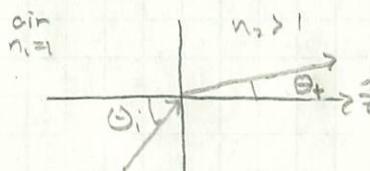
we also have $\vec{k}_t = k_t \sin \theta_t \hat{x} + k_t \cos \theta_t \hat{z}$
+ setting $k_{tx} = k_{ix}$ gives

$$3. \frac{\sin \theta_t}{\sin \theta_i} = \frac{k_t}{k_i} = \frac{v_2}{v_1} = \frac{\lambda_2}{\lambda_1} \quad \text{Snell's Law.}$$

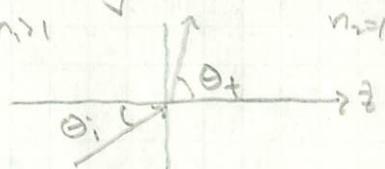
If a wave goes from air wl $n_1 = 1$, to another medium wl $n_2 \geq 1$,

$$\sin \theta_t = \frac{1}{n_2} \sin \theta_i \Rightarrow \theta_t < \theta_i$$

the wave bends towards the normal:



If a wave goes from $n_1 > 1$ to air; $n_2 = 1$, $\theta_t > \theta_i$



Note that in this case, there exists an incident angle $\theta_i = \Theta_i$ that leads to a transmitted angle of $\theta_t = \pi/2$:

$$\sin \theta_t = n_1 \sin \theta_i \Rightarrow \sin \theta_i = \frac{1}{n_1}$$

? What happens after that?

Boundary Conditions

$$\epsilon_1 [\tilde{E}_{oi} + \tilde{E}_{or}]_z = \epsilon_2 [\tilde{E}_{ot}]_z \quad (\perp)$$

$$[\tilde{E}_{oi} + \tilde{E}_{or}]_{xy} = [\tilde{E}_{ot}]_{xy} \quad (\parallel)$$

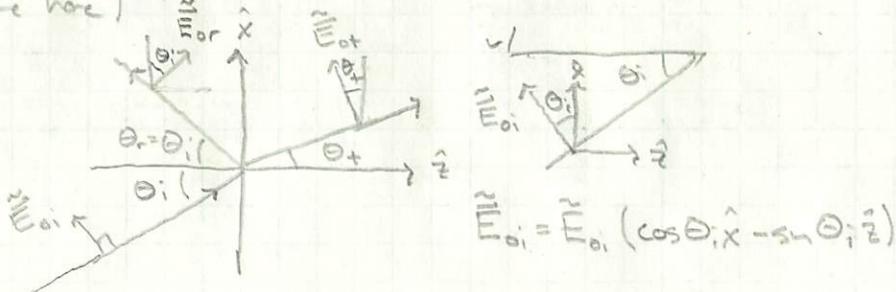
$$[\tilde{B}_{oi} + \tilde{B}_{or}]_z = [\tilde{B}_{ot}]_z \quad (\perp)$$

$$\frac{1}{\mu_1} [\tilde{B}_{oi} + \tilde{B}_{or}]_{xy} = \frac{1}{\mu_2} [\tilde{B}_{ot}]_{xy} \quad (\parallel)$$

w/ $\tilde{B}_{oi} = \frac{1}{v_1} \hat{k}_1 \times \tilde{E}_{oi}$, $\tilde{B}_{or} = \frac{1}{v_1} \hat{k}_r \times \tilde{E}_{or}$

$$\tilde{B}_{ot} = \frac{1}{v_2} \hat{k}_t \times \tilde{E}_{ot}$$

consider the case in which the polarization vector is in the plane of incidence (the xz plane here)



$$\text{and } \sin \tilde{E}_{or} = \tilde{E}_{or} [\cos \theta_i \hat{x} + \sin \theta_i \hat{z}]$$

$$\tilde{E}_{ot} = \tilde{E}_{ot} [\cos \theta_t \hat{x} - \sin \theta_t \hat{z}]$$

then the \perp eqn. for \tilde{E} gives:

$$\epsilon_1 (-\tilde{E}_{oi} \sin \theta_i + \tilde{E}_{or} \sin \theta_i) = \epsilon_2 \tilde{E}_{ot} \sin \theta_t$$

& the \parallel eqn. for \tilde{E} says:

$$\tilde{E}_{oi} \cos \theta_i + \tilde{E}_{or} \cos \theta_i = \tilde{E}_{ot} \cos \theta_t$$

the \parallel \tilde{B} eqn. yields

$$\frac{1}{\mu_1 v_1} (\tilde{E}_{oi} - \tilde{E}_{or}) = \frac{1}{\mu_2 v_2} \tilde{E}_{ot}$$

$$\text{let } \beta = \frac{\mu_1 v_1}{\mu_2 v_2} \quad \alpha = \frac{\cos \theta_t}{\cos \theta_i}$$

$$\text{then } \tilde{E}_{or} = \left(\frac{\alpha - \beta}{\alpha + \beta} \right) \tilde{E}_{oi}; \quad \tilde{E}_{ot} = \frac{2}{\alpha + \beta} \tilde{E}_{oi}$$

to Fresnel eqns