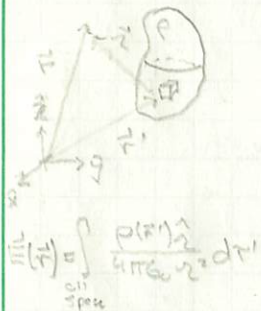


Lost Time



$$\oint \vec{E} \cdot d\vec{A} = \int \frac{\rho(r')}{4\pi\epsilon_0 r'^2} d\tau'$$

If we take $\vec{E} = -\nabla V$ then $\nabla \times \vec{E} = 0$ automatically,

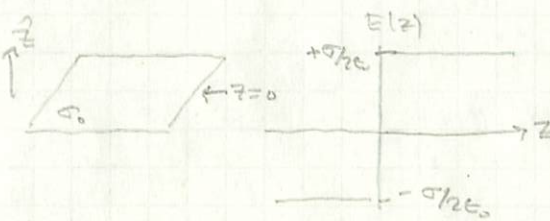
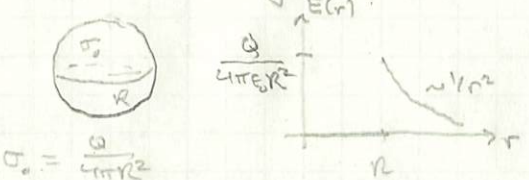
$$\nabla^2 V = -\rho/\epsilon_0 \text{ w/ soln.}$$

$$V(\vec{r}) = \int \frac{\rho(\vec{r}')}{4\pi\epsilon_0 r} d\tau'$$

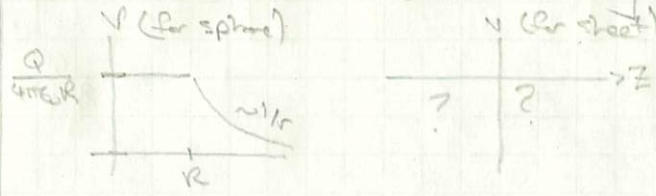
easier integral (to solve!)

Properties of V & E

The electric field suffers a discontinuity at surface charges.

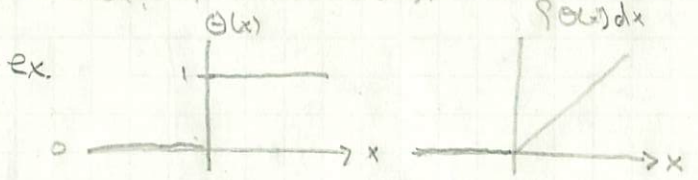


The electrostatic potential V does not have discontinuities at surface charges



Since $\vec{E} = -\nabla V$, V is related to \vec{E} by an integral ($V(\vec{r}) = V(\vec{r}') - \int \vec{E} \cdot d\vec{l}$)

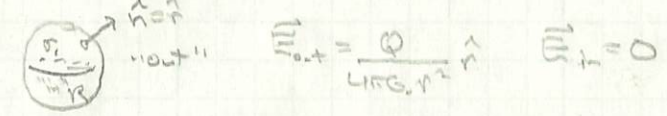
The integral of a discontinuity, like a step function, is continuous:



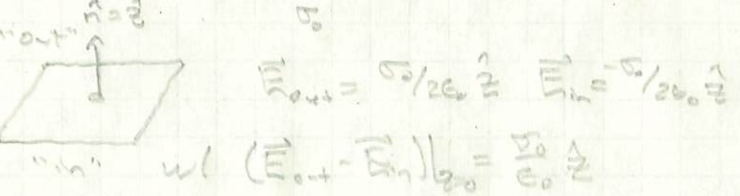
incidentally, that observation helps us understand what happens to \vec{E} at a discontinuity in $\rho \dots$

Discontinuity of E at surface charge

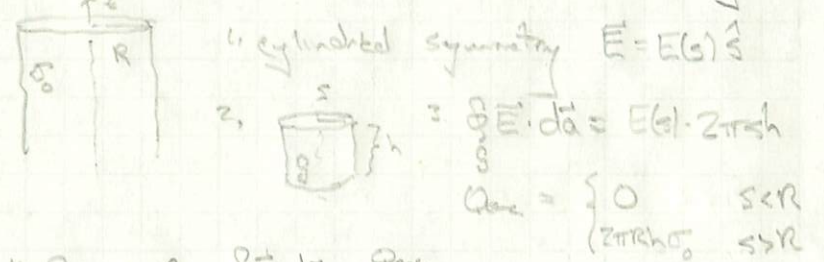
We have 2 examples to for:



$$(\vec{E}_{out} - \vec{E}_{in}) \cdot \hat{n} = \frac{Q}{4\pi R^2} \frac{1}{\epsilon_0} \hat{n} = \frac{\sigma_0}{\epsilon_0} \hat{n}$$



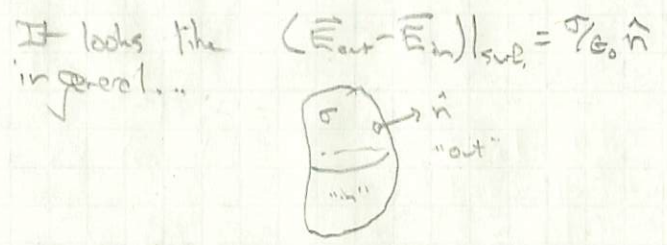
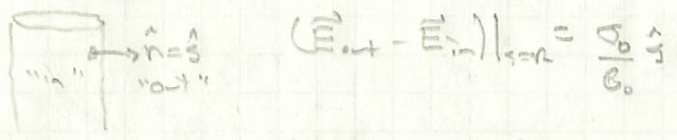
Let's check another example - find \vec{E} for cylinders:



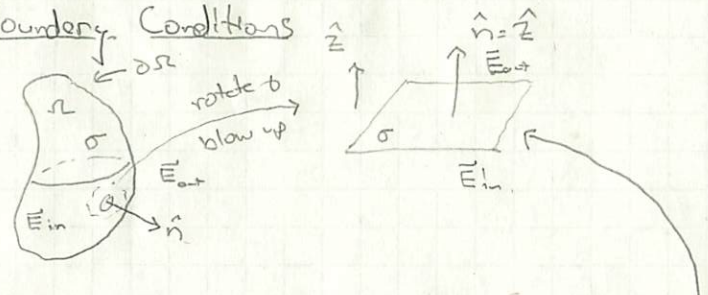
$$\oint \vec{E} \cdot d\vec{a} = \frac{Q_{enc}}{\epsilon_0} = E(s) \cdot 2\pi s h = 0 \Rightarrow \vec{E}_{in} = 0$$

For $s > R$, $\oint_S \vec{E} \cdot d\vec{a} = \frac{Q_{enc}}{\epsilon_0}$
 $E(s) \cdot 2\pi s h = \frac{2\pi R h \sigma}{\epsilon_0}$

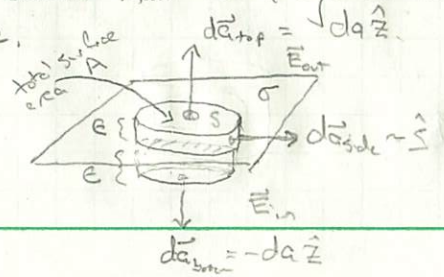
$\vec{E}_{out} = \frac{\sigma R}{\epsilon_0 s} \hat{s}$



Boundary Conditions



apply Gauss's law to a cylinder straddling this surface.



Gauss's Law is $\oint_S \vec{E} \cdot d\vec{a} = \frac{Q_{enc}}{\epsilon_0}$
 at the surface, \vec{E} has components \parallel to \perp to the surface

$\vec{E} = \vec{E}^{\parallel} + \vec{E}^{\perp}$
 $\hat{x} \hat{y} \hat{z}$

let's compute the integral over the surface:

$\oint_S \vec{E} \cdot d\vec{a} = \int_{top} \vec{E}_{out} \cdot d\vec{a}_{top} + \int_{bottom} \vec{E}_{in} \cdot d\vec{a}_{bottom} + \int_{side} \vec{E} \cdot d\vec{a}_{side}$
 $\int_{top} \vec{E}_{out} \cdot d\vec{a}_{top} = \int_{top} \vec{E}_{out}^{\perp} \cdot da \hat{z} = E_{out}^{\perp} A$
 $\int_{bottom} \vec{E}_{in} \cdot d\vec{a}_{bottom} = - \int_{bottom} \vec{E}_{in}^{\perp} \cdot da \hat{z} = -E_{in}^{\perp} A$
 as $\epsilon \rightarrow 0$, this term will vanish for small A

The charge enclosed by the cylinder is $Q_{enc} = \sigma A$
 so

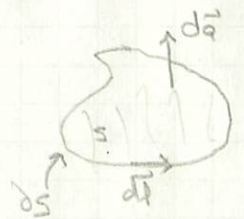
$\lim_{\epsilon \rightarrow 0} \oint_S \vec{E} \cdot d\vec{a} = \frac{\sigma A}{\epsilon_0} \Rightarrow (E_{out}^{\perp} - E_{in}^{\perp})|_{surf} \cdot A = \frac{\sigma A}{\epsilon_0}$
 or $(E_{out}^{\perp} - E_{in}^{\perp})|_{surf} = \sigma/\epsilon_0$ discontinuous \perp component

What about the parallel components of \vec{E} - here, the x & y pieces?

Potential

We can use $\nabla \times \vec{E} = 0$ to find out what happens to the field in the \parallel directions

Note that

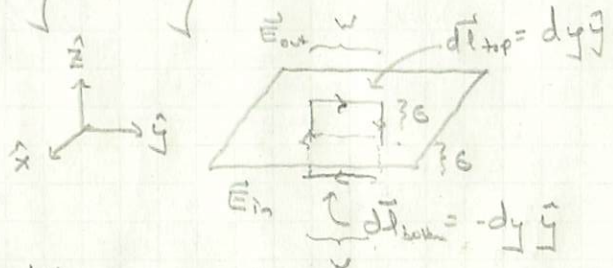


$$\oint (\nabla \times \vec{E}) \cdot d\vec{a} = 0$$

"Stokes's Thm."

$$\oint \vec{E} \cdot d\vec{l} = 0$$

Now for our zoom-in surface, orient a loop w/ legs of height ϵ



For this loop, we have:

$$\oint \vec{E} \cdot d\vec{l} = \int \vec{E}_{out} \cdot d\vec{l}_{top} + \int \vec{E}_{in} \cdot d\vec{l}_{bottom} + \int \vec{E} \cdot d\vec{l}_{sides} = 0$$

this term will go to zero as $\epsilon \rightarrow 0$.

For small w , we have

$$\lim_{\epsilon \rightarrow 0} \oint \vec{E} \cdot d\vec{l} = (\vec{E}_{out}^y w - \vec{E}_{in}^y w) /_{surf} = 0 \quad \text{+ sur. for } \hat{x}\text{-oriented loop.}$$

or

$$(\vec{E}_{out}^y - \vec{E}_{in}^y) /_{surf} = 0 \quad \text{parallel components are continuous}$$

The potential $V(\vec{r})$ is continuous everywhere, but has a discontinuous derivative ∇ - using $\vec{E} = -\nabla V$ in (*)

$$-(\nabla V_{out} - \nabla V_{in}) /_{surf} = \frac{\sigma}{\epsilon_0} \hat{n}$$

dot \hat{n} into both sides:

$$\left(\frac{\partial V_{out}}{\partial n} - \frac{\partial V_{in}}{\partial n} \right) /_{surf} = -\frac{\sigma}{\epsilon_0}$$

$$\text{w/ } \frac{\partial V}{\partial n} /_{surf} = \nabla V \cdot \hat{n} /_{surf}$$

Together: $(\vec{E}_{out} - \vec{E}_{in}) /_{surf} = \sigma / \epsilon_0 \hat{n} \quad \checkmark \quad (*)$